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CONTENT

| Iryna Humeniuk, Angelina Roliak, Oksana Maksymets, Inna Nazarenko | |
|--|-----|
| CASE STUDY AT ESP CLASSES AS MODE OF LANGUAGE ADAPTATION TO | |
| FUTURE ENGINEERING PROFESSION | 15 |
| Iryna Humeniuk, Anastasiia Trofymenko, Alina Kruk, Iryna Melnyk | |
| VIRTUAL EDUCATION SPACE AT ESP CLASSES: CHALLENGES AND | 2.1 |
| PERSPECTIVES | 21 |
| Florin Nenciu, Costin Mircea, Iulian Voicea, Radu Ciuperca, Vlad Arsenoaia | |
| RESEARCH ON NOVEL PLANTING SYSTEM DESIGNED FOR AFFORESTATION OF DESERTIFIED LANDS | 28 |
| Karlis Bickovskis, Valters Samariks, Aris Jansons | 20 |
| EFFECT OF FOREST STAND THINNING ON TREE BIOMASS CARBON STOCK | 36 |
| Ivan Openko, Oleksandr Shevchenko, Yanina Stepchuk, Ruslan Tykhenko, | 50 |
| Olha Tykhenko, Anastasiia Horodnycha | |
| ECONOMIC EFFICIENCY OF METHODS FOR SURVEYING RURAL | |
| INFRASTRUCTURE: ASSESSMENT OF ACCURACY, COST AND DURATION | 42 |
| Inna Savytska, Oksana Bulgakova, Lesya Zbaravska, Iryna Mushenyk, Adolfs Rucins | |
| USE OF INNOVATIVE DIGITAL EDUCATION TECHNOLOGIES IN HIGHER | |
| SCHOOL DURING DISTANCE LEARNING | 48 |
| Inna Savytska, Oksana Bulgakova, Lesya Zbaravska, Mykhailo Torchuk, Adolfs Rucins | |
| PROFESSIONALLY ORIENTED LABORATORY PRACTICUM IN PHYSICS FOR | |
| ENGINEERING STUDENTS | 55 |
| Inna Savytska, Oksana Bulgakova, Lesya Zbaravska, Adolfs Rucins, Mykhailo Torchuk, | |
| Olena Podobied IMPLEMENTATION OF PROFESSIONAL ORIENTATION OF THEORETICAL | |
| TRAINING IN PHYSICS FOR STUDENTS OF ENGINEERING AND PEDAGOGICAL | |
| SPECIALTIES | 63 |
| Oksana Bulgakova, Inna Savytska, Lesya Zbaravska, Adolfs Rucins | |
| PHYSICAL TASKS AND THEIR FUNCTIONS IN TRAINING FUTURE SPECIALISTS | |
| IN AGRICULTURAL AND TECHNICAL INDUSTRY | 70 |
| Volodymyr Ivanyshyn, Oksana Bialkovska, Serhii Yermakov, Oleksii Sikora, Serhiy Oleksiyko | |
| INFLUENCE OF MISCANTHUS BIOMASS TORREFACTION PARAMETERS ON | |
| TORREFIED PRODUCT QUALITY CHARACTERISTICS | 79 |
| Rashmi Jaymin-Sanchaniya, Dany Thomson, Antra Kundzina, Ineta Geipele | |
| EFFECTIVE PROJECT MANAGEMENT PRACTICES IN CONSTRUCTION | 0.5 |
| INDUSTRY: QUANTITATIVE STUDY | 85 |
| Oleksandr Voinalovych, Oleg Hnatiuk, Vasyl Khmelovskyi, Mykhailo Motruch IMPROVEMENT OF OCCUPATIONAL SAFETY AND HEALTH MANAGEMENT | |
| SYSTEM IN UKRAINE IN VIEW OF RELEVANT DECLARED INITIATIVES OF | |
| EUROPEAN UNIONEW OF RELEVANT DECLARED INTIATIVES OF | 93 |
| Kestutis Romaneckas, Ausra Sinkeviciene, Austeja Svereikaite, Rasa Kimbirauskiene, | 73 |
| Kristijonas Vitulskis, Jovita Balandaite, Ugnius Ginelevicius | |
| MAIZE-LEGUME INTERCROPPING EFFECT ON SOIL PROPERTIES AND CO ₂ | |
| CONCENTRATION | 99 |
| Oleg Zagurskiy, Liliya Savchenko, Alona Ohiienko, Svetlana Zagurska, Oleksandr Domin | |
| METHODOLOGY FOR THE FORMATION OF THE COMPANY'S LOGISTICS | |
| SERVICE SYSTEM | 105 |
| Karlis Amatnieks, Aivars Birkavs | |
| EFFECT OF STEAM INJECTION ON PERFORMANCE AND EMISSIONS OF | 112 |
| AGRICULTURAL DIESEL ENGINE | 113 |

| Yinfu Wang, Huili Gao SIMULTANEOUS DETERMINATION OF NINE METAL ELEMENTS IN RIVER SEDIMENTS AND SURROUNDING SOIL BY ICP-MS WITH QUADRUPOLE | |
|--|-----|
| COLLISION CELL TECHNOLOGY | 119 |
| Ilgar Jafarli, Arturs Macanovskis, Eirik Gjerlow, Iveta Novakova, Riho Motlep, Mindaugas Vaisnoras | |
| MECHANICAL PROPERTIES OF EPOXY AND CONCRETE BASED COMPOSITE MATERIALS REINFORCED WITH OIL SHALE ASH | 124 |
| Volodymyr Nazarenko, Victor Smolii, Borys Onyshchenko, Maksym Misiura SYSTEM MODEL OF E-SERVICES FOR SUBURBAN AREA MANAGEMENT | 135 |
| Juris Hazners EVALUATION OF SOCIO-ECONOMIC IMPACT OF LATVIAN MUNICIPAL ADJUSTMENT FUND WITH REGRESSION DISCONTINUITY DESIGN MODEL | 142 |
| Adolfs Rucins, Dainis Viesturs TRENDS IN DEVELOPMENT OF GRAIN COMBINE HARVESTER FLEET IN LATVIA | 149 |
| Vaidas Bivainis, Egle Jotautiene, Ramunas Mieldazys, Grazvydas Juodisius SIMULATION RESEARCH ON PROPERTIES OF SPHERICAL MANURE GRANULES | 155 |
| Dainis Berjoza, Inara Jurgena, Jiri Masek CHANGES IN ELECTRIC CAR ENERGY CONSUMPTION DEPENDING ON MASS | 161 |
| Sanjay-Rajni Vejanand, Alexander Janushevskis, Ivo Vaicis ANALYZING EFFICIENCY OF VENTILATION ELEMENTS USED IN PROTECTIVE CLOTHING WITH SIMPLIFIED MODEL | 169 |
| Miroslaw Rucki, Edvin Hevorkian, Boranbay Ratov, Volodymyr Mechnik STUDY ON PROPERTIES OF ZIRCONIA REINFORCED REFRACTORY MATRIX COMPOSITES | |
| Raimonds Valdmanis, Maija Zake KINETIC STUDY ON MICROWAVE PRE-TREATED BIOMASS COMBUSTION, HEAT PRODUCTION AND EMISSION COMPOSITION | |
| Marcin Kisiel, Dariusz Szpica EVALUATING INFLUENCE OF CFD MESH ON FLOW CHARACTERISTICS OF PNEUMATIC BRAKE VALVE DIFFERENTIAL SECTION | 190 |
| Oksana Bulgakova, Inna Savytska, Lesya Zbaravska, Ilmars Dukulis, Mykhailo Torchuk, Adolfs Rucins, Oksana Zakhutska FORMATION OF PROFESSIONAL COMPETENCE OF FUTURE AGRICULTURAL ENGINEERING SPECIALISTS STUDYING DISCIPLINE ""MAINTENANCE OF MACHINERY AND EQUIPMENT"" | 196 |
| Oksana Bulgakova, Inna Savytska, Lesya Zbaravska, Ilmars Dukulis, Adolfs Rucins FORMATION OF SELF-EDUCATIONAL COMPETENCE OF FUTURE ENGINEERS AS CONTEMPORARY PEDAGOGICAL PROBLEM | |
| Volodymyr Didukh, Igor Tsiz, Vasyl Satsiuk, Roman Khlopetscyi RESEARCH IN PROCESSES AND MACHINES FOR LOCAL STRIP APPLICATION OF MOISTURE-HOLDING ORGANIC FERTILIZERS | 212 |
| Manfred Sneps-Sneppe, Dmitry Smirnov ABOUT IRR AND NEW INVESTMENT PRIORITY INDEX | |
| Anton Koshel, Iryna Kolhanova, Ruslan Tykhenko, Ivan Openko ECOLOGICAL AND ECONOMIC ASSESSMENT OF EFFECTIVENESS OF DISTURBED LAND RECLAMATION IN UKRAINE | |
| Daria Vakulenko, Viktor Mileikovskyi, Tetiana Tkachenko, Oleksandr Liubarets INVESTIGATION IN CRITICAL RADIUS OF THERMAL INSULATION FOR VERTICAL PIPES | 232 |
| Wei Yu, Yuqing Chen, Shitong Zhou, Qianchen Zhou RESEARCH ON HIGHLIGHT RESTORATION ALGORITHM FOR SEA | 230 |

| Egle Jotautiene, Antanas Juostas, Atilgan Atilgan INVESTIGATION ON ENVIRONMENTALLY FRIENDLY WHEAT HARVEST TECHNOLOGY | . 245 |
|--|-------|
| Viktor Sheichenko, Serhii Koropchenko, Oleksandr Horbenko, Yuliia Skoriak, Denys Sheichenko RESULTS OF RESEARCH ON FACTORS INTENSIFYING HEMP TRUST | |
| PREPARATION PROCESSES | . 251 |
| Abdulkadr Ahmed Abduletif, György Neszmelyi, Henrietta Nagy ROLE OF TRANSPORT INFRASTRUCTURE IN THE ETHIOPIAN ECONOMY | . 258 |
| Pavels Patlins SMALL SHIPMENT SUSTAINABLE DELIVERIES WITHIN AND BETWEEN CITIES | . 263 |
| Yurii Franchuk, Viktoriia Konovaliuk, Mykhailo Kyrychenko, Oleksandr Liubarets JUSTIFICATION OF MEASURES TO IMPROVE STABILITY OF GAS DISTRIBUTION NETWORKS | . 271 |
| Atilgan Atilgan, Firat Arslan, Burak Saltuk, Joanna Kociecka, Egle Jotautiene, Antanas Juostas EFFECTS OF VERMICOMPOST APPLICATION ON GROWTH AND YIELD OF HOT PEPPER (<i>CAPSICUM FRUTESCENS</i>) | . 280 |
| Jacek Caban, Aleksander Nieoczym, Leszek Krzywonos STRENGTH ANALYSIS OF SUBSOILER TOOTH | . 286 |
| Jacek Caban, Jaroslaw Senko, Tomasz Slowik, Szymon Dowkontt PRELIMINARY STUDY OF THE STARTING SYSTEM THROUGH THE ELECTRICAL PARAMETERS OF THE START-UP PROCESS OF THE DIESEL ENGINE | . 294 |
| Taliat Azizov, Nataliia Sribniak, Liudmyla Tsyhanenko, Dmytro Volkov MODELLING OF REINFORCED CONCRETE SLAB TO ACCOUNT FOR CRACKING | . 302 |
| Kithalawalana Jayathilaka, Oskars Gainutdinovs, Svetlana Sokolova, Peteris Studers STRENGTH ANALYSIS OF FEMORAL IMPLANT OF BONE ANCHORED PROSTHESIS | . 312 |
| Yevhenii Aftandiliants, Svyatoslav Gnyloskurenko, Helena Meniailo, Valerii Khrychikov, Viktor Lomakin INFLUENCE OF K ₂ ZRF ₆ AND SIO ₂ ON REFINING ABILITY OF FLUX FOR MANUFACTURING BIMETALLIC CASTINGS | . 319 |
| Daria Vakulenko, Tetiana Tkachenko, Viktor Mileikovskyi, Viktoriia Konovaliuk, Oleksandr Liubarets TIGHTNESS MONITORING CAMERA FOR CRITICAL PARTS OF RURAL TECHNOLOGICAL AND SCIENTIFIC EQUIPMENT | 226 |
| Aleksej Mironov, Pavel Doronkin, Vitalijs Kuzmickis, Aleksejs Safonovs SENSOR NETWORK APPLICATION FOR STUDYING MODAL PROPERTIES OF TURBOMACHINE | |
| Astra Auzina-Emsina, Alberts Auzins MODELLING OF DEMAND SHOCK IMPACT IN FOOD SECTOR ON SECTORAL DEVELOPMENT: CASE OF LATVIA | . 338 |
| Vitalijs Beresnevich, Janis Viba, Edgars Kovals, Martins Irbe, Maris Eiduks LATERAL SWAY MOTION OF VEHICLE AND TRAILER | . 344 |
| SerhiÑ– Yukhymchuk, Svitlana Yukhymchuk, Mykola Tolstushko, Nataliya Tolstushko CHECKING PERFORMANCE OF DISC-BELT FLAX PULLING APPARATUS | . 351 |
| Stasys Slavinskas, Paulius Bendziunas EXPERIMENTAL STUDY ON INFLUENCE OF BIOFUELS ON INJECTION CHARACTERISTICS OF DIESEL ENGINE COMMON RAIL SYSTEM | . 357 |
| SerhiÑ– Khomych, Igor Tsiz, Victor Tarasyuk, Roman Khlopetscyi DEVELOPMENT OF METHOD AND STUDY OF GRANULAR FERTILIZER PRODUCTION PROCESS BASED ON SAPROPEL | . 363 |

| Savelii Kukharets, Algirdas Jasinskas, Olena Sukmaniuk, Mykolai Kukharets | |
|--|------|
| ENERGY CONVERSION OF BIOMASS FROM FAST-GROWING PLANTS FOR HEAT PRODUCTION | 369 |
| Olena Khomenko, Viktoriia Ivchenko, Ludmyla Boginska, Galina Fomenko | |
| PROTECTIVE COATINGS FOR CONSTRUCTION CERAMICS AS FACTOR OF | |
| INCREASING ENERGY EFFICIENCY AND OPERATIONAL PROPERTIES OF PRODUCTS | 375 |
| Tatjana Sinkus, Inese Ozola | |
| ENGINEERING STUDENT PERCEPTIONS OF AI TECHNOLOGY | |
| IMPLEMENTATION IN ESP | 381 |
| Jozsef Kaposzta, Balazs Lorinc | |
| ECONOMIC ANALYSIS OF EMERGENCE OF BIPOLAR EUROPEAN UNION, | 200 |
| 2011-2022 | 390 |
| Balazs Lorinc, Jozsef Kaposzta EXAMINING SPATIAL DIFFERENCES IN HIGH-PRESTIGE EMPLOYMENT IN | |
| HUNGARY, 2011-2022 | 396 |
| Valerijs Skribans, Natalia Maslii, Maryna Demianchuk | |
| CASE STUDY OF GRAIN EXPORT ROUTS CHANGES FOR UKRAINE IN 2022-2023 | 402 |
| Radovan Madlenak, Lucia Madlenakova, Henrietta Nagy, Gyorgy Neszmelyi | |
| EXPERIMENTAL TESTING OF CONSUMER BRAND ENGAGEMENT: | |
| EVALUATING HIGH-VALUE TECHNOLOGY BRANDS THROUGH EYE TRACKING METHODOLOGY | 400 |
| | 408 |
| Astra Auzina-Emsina GREENER LAST-MILE DELIVERY TECHNOLOGIES AND REGIONAL | |
| DEVELOPMENT IN LATVIA: INPUT-OUTPUT APPROACH | 414 |
| Astra Auzina-Emsina, Inguna Jurgelane-Kaldava, Agnese Batenko, Linda Kelle | |
| TRANSPORT SECTOR TECHNOLOGICAL SHIFTS AND INTERSECTORAL | |
| LINKAGES IN LATVIA | 422 |
| Dmitrij Morozow MODIFICATION OF CUTTING TOOL SURFACES WITH ION IMPLANTATION | 120 |
| Dmitrijs Gorbacovs, Pavels Gavrilovs, Janis Eiduks | 420 |
| MODELLING OF HAZARDOUS OPERATING MODES OF RUBBER-CORD | |
| COUPLING IN FEM ENVIRONMENT | 434 |
| Vasyl Petrenko, Oksana Naumenko, Oksana Nechai, Valeria Bondar | 4.40 |
| WAR INFLUENCE ON SUNFLOWER SEED AND OIL PRODUCTION IN UKRAINE | 442 |
| Nataliia Sribniak, Valerii Lutskovskyi, Liudmyla Tsyhanenko, Serhii Halushka, Hennadii Tsyhanenko, Stanislav Rohovyi | |
| REGULATION OF SPACE GRID STRUCTURE STRESS-STRAIN STATE | 448 |
| Edgars Buksans, Ilze Kalnina | |
| IMPROVEMENT OF REACTION TO FIRE PERFORMANCE OF BIRCH PLYWOOD | |
| BY VENEER SOAKING METHOD | 460 |
| Vasyl Khmelovskyi, Roman Vasylenko, Victor Rebenko, Svitlana Potapova INTENSIFICATION OF STEM MATERIAL SHREDDING PROCESS | 167 |
| | 46 / |
| Mohamed H. Shaban, Hassan Mohammad Ali DEVELOPING A BIM-BASED TECHNIQUE IN THE DESIGN PHASE TO ACHIEVE | |
| SUSTAINABILITY IN RESIDENTIAL BUILDING PROJECTS | 474 |
| Victor Zaharchuk, Oleh Zaharchuk, Mykola Tolstushko, Nataliya Tolstushko | |
| IMPROVING PERFORMANCE OF WHEELED TRACTOR WITH GAS ENGINE AS | |
| PART OF TRANSPORT MACHINE UNIT | 488 |
| Olha Tykhenko, Andrii Martyn, Ruslan Tykhenko, Ivan Openko | |
| CADASTRAL ACCOUNTING OF LAND PLOTS AS INFORMATION BASIS | 105 |

| Waldemar Samociuk, Pawel Staczek PRECISION AIR SEEDER FOR HEMP - CONTROL SYSTEM SIMULATION | 501 |
|--|------|
| Eshpulat Eshdavlatov, Akmal Eshdavlatov, Maxmatmurod Shomirzaev, Nurmuxammad Xamidov | |
| PHYSICAL-MECHANICAL PROPERTIES OF ONION SEEDS AND SOIL | 507 |
| Volodymyr Bulgakov, Aivars Aboltins, Valerii Adamchuk, Volodymyr Kuvachov, V olodymyr Kyurchev, Adolfs Rucins, Oleh Chernysh | |
| INVESTIGATION OF WIDE SPAN VEHICLE TECHNOLOGICAL PART SUSPENSION SYSTEM COMPACTING IMPACT ON SOIL | 513 |
| Volodymyr Bulgakov, Aivars Aboltins, Valerii Adamchuk, Volodymyr Kuvachov, Simone Pascuzzi, Volodymyr Kyurchev, Adolfs Rucins, Victor Nesvidomin | |
| INVESTIGATION OF WIDE SPAN VEHICLE TECHNOLOGICAL PART MOVEMENT STABILITY | 522 |
| Alberts Auzins, Aivars Aboltins, Andris Lismanis IDENTIFICATION OF EXTERNAL SHOCK IMPACT ON AGRI-FOOD SECTOR BY | |
| APPLYING OUTLIER DETECTION TESTS: CASE OF LATVIA | 531 |
| Zbigniew Krzysiak PROFITABILITY OF SUGAR BEET PRODUCTION IN 2023/2024 CAMPAIGN ON | - 40 |
| EXAMPLE OF LUBLIN VOIVODESHIP | 540 |
| Ivars Kudrenickis, Gaidis Klavs, Janis Rekis POTENTIAL OF RENEWABLE ENERGY COMMUNITIES IN LATVIA€™S ENERGY SECTOR TRANSFORMATION | 550 |
| Vilis Dubrovskis, Imants Plume BIOGAS POTENTIAL FROM BIODIESEL PRODUCTION RESIDUES | |
| Vilis Dubrovskis, Imants Plume BIOMETHANE PRODUCTION FROM PELLETS OF HORSE MANURE AND LITTER MIXTURE | 564 |
| Vilis Dubrovskis, Dagnis Dubrovskis METHANE PRODUCTION FROM BIRCH AND MAPLE LEAVES AND MISCANTHUS GRASS | |
| Michal Ballay, Ludmila Macurova, Pavol Kohut, Miroslav Redl | 507 |
| INFLUENCE OF ROAD USER BEHAVIOR ON OCCURRENCE OF ACCIDENT: AGRICULTURAL VEHICLES AND MOTORCYCLISTS | 574 |
| Elina Konstantinova, Andis Lazdins, Imants Kruze | |
| FUNCTIONAL LAND MANAGEMENT MODEL - TOOL FOR SUSTAINABLE AND CLIMATE FRIENDLY MANAGEMENT OF NUTRIENT RICH ORGANIC SOILS | 580 |
| Iryna Romanenko, Iveta Novakova, Riho Motlep, Volodymyr Gulik, Andrejs Krasnikovs, Mindaugas Vaisnoras | |
| NEUTRON SHIELDING MATERIAL CONTAINING BASALT-BORON FIBERS AND OSA FOR SPENT NUCLEAR FUEL CONTAINER, NUMERICAL MODELLING | 588 |
| Vytautas Adomavicius, Gintvile Simkoniene, Artem Dedenok | 500 |
| POSSIBILITIES AND BENEFITS OF USING PHOTOVOLTAIC POWER PLANTS WITH MICROINVERTERS IN RURAL AREAS | 594 |
| Vytautas Adomavicius, Gintvile Simkoniene, Artem Dedenok USEFULNESS OF SMALL-SCALE STAND-ALONE HYBRID SOLAR-WIND POWER PLANTS IN RURAL AREAS | 601 |
| Andrii Martyn, Liudmyla Hunko, Liudmyla Kolosa, Nataliia Medynska, Anatolii Poltavets | 001 |
| RESILIENCE IN FACE OF ADVERSITY: ASSESSING RUSSIAN AGGRESSION IMPACT ON LAND SURVEYING ENGINEERING SECTOR IN UKRAINE | 608 |
| Yurii Chovniuk, Anna Moskvitina, Mariia Shyshyna, Serhii Rybachov, Olha Mykhailyk OPTIMIZATION OF HEAT TRANSFER PROCESSES IN ENCLOSING STRUCTURES | |
| OF ARCHITECTURAL MONUMENTS LOCATED OUTSIDE URBAN AGGLOMERATION | 615 |

| Yurii Chovniuk, Anna Moskvitina, Serhii Rybachov, Petro Zinych NONISOTHERMAL FLOW OF NANOFLUID IN GROUND HEAT ACCUMULATOR | |
|---|-----|
| FOR DECENTRALIZED HEAT SUPPLY OF RURAL FACILITIES FOR VARIOUS PURPOSES | 623 |
| Tabita Treilande, Ilmars Iltins NON-STANDARD METHOD FOR SOLVING HYPERBOLIC HEAT EQUATIONS | 630 |
| Jan Dizo, Alyona Lovska, Miroslav Blatnicky, Vadym Ishchuk, Denis Molnar DERIVATION OF MATHEMATICAL MODEL OF MECHANISM FOR DRIVE OF TRANSPORT MEANS ADDITIONAL DEVICE | 636 |
| Algirdas Jasinskas, Rita Petlickaite, Marius Praspaliauskas, Kestutis Romaneckas, Ausra Sinkeviciene IMPACT OF ASH OBTAINED AFTER MULTI-CROP PELLET BURNING ON SPRING | |
| BARLEY FERTILIZATION | |
| Umesh Vavaliya, Ilgar Jafarli, Olga Kononova, Iveta Novakova, Riho Motlep INVESTIGATION OF UD HIBRIDE BASALT FIBER/EPOXY COMPOSITE MECHANICAL PROPERTIES DEPENDING ON LENGTH | 657 |
| Imants Plume, Eduards Azits, Vilis Dubrovskis, Lauris Plume PRODUCTION OF BIOGAS FROM GRASS AT VARIOUS PRE-TREATMENT AND ANAEROBIC FERMENTATION TEMPERATURES UNDER INFLUENCE OF MAGNETIC FIELD | |
| Vladislav Yaroshevsky, Igor Bespalov, Vasyli Khodorchuk, Vitalii Barkar, Volodymyr Bulgakov, Adolfs Rucins, Aivars Aboltins EXPERIMENTAL STUDY OF LARVAE CAGE AREA IMPACT ON OUTPUT IN GREEN LACEWING INDUSTRIAL-SCALE REARING | |
| Zaiga Anna Zvaigzne, Dana Purvina, Raitis Normunds Melniks, Aldis Butlers, Andis Lazdins SOIL CARBON TURNOVER OF DRAINED AND NATURALLY WET MINERAL FOREST SOILS IN LATVIA | 678 |
| Volodymyr Bulgakov, Ivan Holovach, Volodymyr Martyniuk, Oleksandra Trokhaniak, Aivars Aboltins, Adolfs Rucins, Yevhen Ihnatiev MATHEMATICAL MODEL OF MOVEMENT AND CLEANING BEETROOTS FROM SOIL LUMPS WITH SPIRAL SEPARATOR | |
| Ilona Skranda, Gints Spalva, Edgars Muiznieks, Andis Lazdins COMPARISON OF NITROUS OXIDE (N₂O) AND METHANE (CH₄) FLUXES IN NATURALLY WET AND DRAINED MINERAL FOREST SOIL | |
| Valerii Adamchuk, Viktor Prysyazhnyi, Volodymyr Bulgakov, Hryhorij Kaletnik, Viktor Mazur, Oleksandra Trokhanyak, Aivars Aboltins, Adolfs Rucins, Ivan Holovach INVESTIGATION AND SUBSTANTIATION OF MISCANTHUS RHIZOME DIGGER PIN GRID DESIGN PARAMETERS | 702 |
| Volodymyr Bulgakov, Oleksandra Trokhaniak, Aivars Aboltins, Adolfs Rucins, Mycola Tkachenko, Arlindo Almeida, Volodymyr Kuvachov INVESTIGATION OF CONTACT STRESSES IN ENGAGEMENT ELEMENTS OF SCREW CONVEYOR SAFETY CLUTCH | |
| Volodymyr Bulgakov, Ivan Holovach, Igor Savchenko, Petro Rykhlivskyi, Myroslav Budzanivskyi, Aivars Aboltins, Adolfs Rucins, Juri Olt, Yevhen Ihnatiev THEORETICAL STUDY OF FLEXIBLE BLADE MOVEMENT IN CLEANING CARROT ROOT CROP HEADS WITHOUT EXTRACTING THEM FROM SOIL | 722 |
| Volodymyr Kuzmenko, Oleksandr Kholodyuk, Borys Kotov, Viacheslav Bratishko BEATER-KNIFE CUTTING DEVICES OF FORAGE HARVESTING MACHINES AND WAYS FOR THEIR IMPROVEMENT | 732 |

| Aivars Aboltins, Janis Palabinskis DRYING DYNAMICS OF DIFFERENTLY PREPARED FRESH CRANBERRIES AND | |
|---|------|
| BLUEBERRIES USING IR DRYING | 739 |
| Andrejs Kovalovs, Evgeny Barkanov, Oleksiy Vodka IDENTIFICATION PROCEDURE OF FUNCTIONALLY GRADED MATERIAL IN SANDWICH BEAM | 746 |
| Harijs Kalis, Ilmars Kangro MATHEMATICAL MODELLING OF CHEMICAL REACTION WITH PROPANE | 753 |
| Gunita Mazure ENERGY EFFICIENCY IMPROVEMENT SUPPORT PROGRAMMES FOR PRIVATE BUILDINGS IN LATVIA | 762 |
| Tomasz Mazur EFFECTS OF PART COORDINATE SYSTEM APPOINTMENT ON CMM MEASUREMENT | 769 |
| Vitaliy Tkach, Vasyl Achkevych, Viacheslav Bratishko, Oksana Achkevych JUSTIFICATION OF MACHINE MILKING PHYSIOLOGICAL PRINCIPLES | 775 |
| Guna Petaja, Dana Purvina, Arta Bardule, Zaiga Anna Zvaigzne CH4 AND N2O EMISSIONS FROM SURFACE OF DECIDUOUS TREE STEMS IN FORESTS WITH DRAINED AND NATURALLY WET MINERAL SOILS | |
| Olha Chaikovska, Maryna Voloshchuk, Liudmyla Komarnitska, Oksana Palyliulko ENHANCING COMMUNICATION SKILLS OF ENGINEERING STUDENTS THROUGH EFL PLATFORM-ASSISTED PROJECT WORK | |
| Ilona Skranda, Dana Purvina, Arta Bardule, Guna Petaja METHANE (CH4) AND NITROUS OXIDE (N2O) EMISSIONS FROM SURFACE OF DECIDUOUS TREE STEMS AND SOIL IN FORESTS WITH DRAINED AND | / 00 |
| NATURALLY WET ORGANIC SOILS Emils Martins Upenieks, Martins Vanags Duka, Aldis Butlers, Andis Lazdins SHOPT TERM SEFECT OF GLEAR FELLING ON GREENHOLISE GAS EMISSIONS | 793 |
| SHORT TERM EFFECT OF CLEAR-FELLING ON GREENHOUSE GAS EMISSIONS FROM NATURALLY WET ORGANIC AND MINERAL SOILS | 800 |
| Ilona Skranda, Gints Spalva, Arta Bardule, Andis Lazdins CASE STUDY ON EFFECT OF REWETTING GRASSLAND WITH ORGANIC SOILS ON GREENHOUSE GAS (GHG) EMISSIONS FROM SOIL | 805 |
| Andriy Novytskyi, Valentyna Melnyk, Oleksandr Banniy, Valeryi BystryÑ–, Serhii Stetsiuk RESEARCH ON INFLUENCE OF GEOMETRIC PARAMETERS OF ENGINE BODY | |
| PARTS DURING REPAIR PROCESS | 811 |
| IN UKRAINE DURING WAR | 817 |
| Frantisek Horejs, Martin Cisler, Libor Matyas, Michal Strnad INFLUENCE OF DISC CULTIVATOR DESIGN ON SOIL PARTICLE DISPLACEMENT | 826 |
| Vasyl Achkevych, Borys Onyshchenko, Iurii Gumeniuk, Oksana Achkevych CONSTRUCTION FEATURES OF POTATO HARVESTERS AND THEIR INFLUENCE ON DAMAGE TO POTATO TUBERS DURING HARVESTING | 832 |
| Martin Cisler, Frantisek Horejs, Michal Strnad, Libor Matyas INFLUENCE OF ORGANIC FERTILIZERS ON SOIL EROSION PARAMETERS IN MAIZE CROP | 838 |
| Uldis Zaimis, Sintija Ozolina, Andrejs Kukuskins WHEAT STRAW AND SEAWEED <i>FURCELLARIA LUMBRICALIS</i> - DERIVED | |
| CARRAGEENAN BIOCOMPOSITE CHARACTERISTICS: CASE STUDY | 844 |
| FORMATION IN UKRAINE (EXAMPLE OF RENEWABLE ENERGY SOURCES) | 850 |

| Natalja Budkina, Gerda Dubkevicha, Aija Pola | |
|--|-----|
| ON HOMEWORK ROLE IN MATHEMATICS TEACHING AT RIGA TECHNICAL UNIVERSITY | 050 |
| Sintija Ozolina, Uldis Zaimis, Andrejs Kukuskins | 030 |
| DEVELOPMENT AND APPLICATION OF BIODEGRADABLE WHEAT STRAW AND | |
| CARRAGEENAN COMPOSITE IN AGRICULTURE | 865 |
| Viktorija Politika, Jelena Pundure, Marina Jarvis | |
| SOLUTIONS FOR REDUCING (MINIMIZING) FIREFIGHTING TRUCK REPAIRS IN | |
| EU COUNTRIES AND IN LATVIA IN PARTICULAR | 870 |
| Michal Strnad, Libor Matyas, Martin Cisler, Petr Novak COMPARISON OF FUEL CONSUMPTION IN BROCCOLI PRODUCTION | 881 |
| Andrejs Stupans, Pavels Maksimkins, Armands Senfelds, Leonids Ribickis | |
| DEVELOPMENT AND TESTING OF AUTOMATED CONTROL SYSTEM FOR SEA | 007 |
| BUCKTHORN BERRY HARVESTING ROBOT ""AGROBOT"" | 887 |
| Matiss Erins, Zigurds Markovics APPLICATION OF TOPOLOGICAL MODELLING METHODS FOR DETERMINING | |
| HUMAN FATIGUE | 894 |
| Karunamoorthy Rengasamy Kannathasan, Stanley Jacob Maria Michaelraj, | |
| Eirik Gjerlow, Iveta Novakova, Mindaugas Vaisnoras | |
| HYBRID FIBER COMPOSITE MATERIAL WITH OSA MECHANICAL LOAD- | |
| BEARING CAPACITY AFTER THERMAL HEATING | 901 |
| Mirela-Nicoleta Dinca, Mariana Ferdes, Gigel Paraschiv, Bianca-Stefania Zabava | |
| ENZYMATIC PRETREATMENT OF LIGNOCELLULOSIC BIOMASS FOR BIOGAS | 008 |
| PRODUCTION - REVIEW | 908 |
| Inga Grinfelde, Kristaps Siltumens, Vilda Grybauskiene, Maris Bertins, Jovita Pilecka-Ulcugaceva | |
| INFLUENCE OF INDUSTRY ON AIR POLLUTION IN JELGAVA CITY | 914 |
| Vladislav Zavadskiy, Gita Revalde | |
| UPCOMING WATER DEFICIT IN CENTRAL ASIA RURAL REGIONS AND | |
| PERSPECTIVES OF GREEN HYDROGEN PRODUCTION | 921 |
| Bohdan Valetskyi, Mykola Tolstushko, Nataliya Tolstushko, Yurii Fedorus | |
| RESEARCH ON OVERSIZED LOAD PACKAGING | 927 |
| Uldis Strautins, Maksims Marinaki | |
| ON SIMULATION OF SOFT MATTER AND FLOW INTERACTIONS IN BIOMASS PROCESSING APPLICATIONS | 022 |
| Kristaps Siltumens, Inga Grinfelde, Ginters Znots, Rudolfs Golubovs, Raitis Brencis | 933 |
| USE OF SHREDDED TEXTILE WASTE AS MATERIAL FOR SOUND ABSORPTION | 939 |
| Sergey Kravchenko, Natalia Kravchenko, Nikolay Kuleshov, Igor Laptinov, | |
| Andrey Kravchenko, Daria Panova | |
| DEVELOPMENT OF LOW TEMPERATURE TRAP FOR CAPTURING VALUABLE | |
| BIOLOGICAL ACTIVE MATERIALS | 946 |
| Olesja Grigorjeva, Zigurds Markovics | |
| ANALYSIS OF CHANGES IN BRAIN MODEL PARAMETERS AFTER STROKE | 954 |
| Svetlana Sokolova, Janis Viba, Vladislavs Jevstignejevs | |
| BIFURCATION ANALYSIS OF DYNAMICAL SYSTEM WITH NONLINEAR DASHPOT AND IMPACTS | 061 |
| Ivan Rogovskii, Igor Sivak, Ruslan Shatrov, Oleksandr Nadtochiy | 901 |
| AGROENGINEERING STUDIES OF TILLAGE AND HARVESTING PARAMETERS IN | |
| SOYBEAN CULTIVATION | 965 |
| Sergey Kravchenko, Natalia Kravchenko, Nikolay Kuleshov, Igor Laptinov, | |
| Andrey Kravchenko, Daria Panova | |
| VACUUM EVAPORATING MACHINE FOR LIQUID PRODUCTS BASED ON | 0=1 |
| FI AMMARI F SOI VENTS | 971 |

| Girts Veigners, Ainars Galins | |
|--|------|
| INTEGRATING ADAPTIVE ARTIFICIAL INTELLIGENCE FOR RENEWABLE | |
| ENERGY FORECASTING: ANALYSIS OF SCIENTIFIC RESEARCH | 1120 |
| Maris Juruss, Baiba Smite-Roke, Irina Nesterenko REDUCING EXTERNALITIES OF LAST MILE DELIVERY THROUGH TAXATION | 1129 |
| Yifang Ling, Guodong Liu, Jun Li, Qiuyun Shi NUMERICAL SIMULATION OF GROUNDWATER POLLUTION IN HILLY AREAS WITH COMPLEX TERRAIN BASED ON GMS | 1137 |
| Serhii Stepanenko, Borys Kotov, Alvian Kuzmych, Iryna Demchuk, Vitaly Melnyk, Daryna Volyk MODELLING OF AERODYNAMIC SEPARATION OF GRAIN MATERIAL IN | 1137 |
| MODELLING OF AEROD I NAMIC SEPARATION OF GRAIN MATERIAL IN COMBINED CENTRIFUGAL-PNEUMATIC SEPARATOR | 1143 |

REVIEWERS

Vytautas Adomavicius, Yevhenii Aftandiliants, Anna Ageicheva, Karlis Amatnieks, Eve Aruvee, Komil Astanakulov, Astra Auzina-Emsina, Anita Auzina, Alberts Auzins, Aivars Aboltins, Dainis Berjoza, Marco Bietresato, Jana Bikovska, Liepa Bikulciene, Aivars Birkavs, Gints Birzietis, Vaidas Briede, Dace Brizga, Natalja Budkina, Volodymyr Bulgakov, Sidona Buragiene, Bivainis, Baiba Andriy Burbelko, Juris Burlakovs, Jacek Caban, Ugis Cabulis, Zanna Cernostana, Chengcheng Xia, Andrejs Cibulis, Aleksandra Cimbale, Dovile Ciuldiene, Mirela - Nicoleta Dinca, Vija Dislere, Ales Dittrich, Jan Dizo, Vasyl Dmytriv, Kumawat Dr. Lokesh, Ilmars Dukulis, Daniela Durcanska, Emad Kadum Njim, Liga Feldmane, Alistair Forbes, Maris Gailis, Ainars Galins, Ilya A. Galkin, Guilin Hu, Sandra Gusta, David Hajek, Juris Hazners, Maria Heldak, Sakke Tira Hendry, Michal Holubcik, Frantisek Horejs, Taras Hutsol, Yevhen Ihnatiev, Ilgar Jafarli, Khanum Jafarova, Algirdas Jasinskas, Petr Jilek, Egle Jotautiene, Ilze Judrupa, Antanas Juostas, Zuhriddin Juraev, Inara Jurgena, Aivars Kakitis, Harijs Kalis, Daina Kanaska, Liene Kancevica, Ilmars Kangro, Gaidis Klavs, Gaidis Klavs, Yevhenii Klymenko, Zafirova Koleta, Vitalijs Komasilovs, Vitalijs Komasilovs, Maros Korenko, Nezihe Korkmaz Guler, Iryna Koshkalda, Oleksandra Kovalyshyn, Oleg Kucher, Inguna Leibus, Arnis Lenerts, Arturs Lesinskis, Oleg Liashuk, Tomasz Lipinski, Jenny Lorio, Renata Macaitiene, Nelson Madonsela, Farmon Murtozevich Mamatov, Maris Mangalis, Ausra Marcinkeviciene, Andrii Martyn, Jonas Matijosius, Libor Matyas, Oleksandr Medvedskyi, Ramunas Mieldazys, Olga Miezite, Senay Mihcin, Kostiantyn Mykhalenkov, Henrietta Nagy, George Naibin, Olena Nalobina, Kestutis Navickas, Gyorgy Ivan Neszmelyi, Cossi Telesphore Nounangnonhou, Jan Ondrus, Inese Ozola, Sintija Ozolina, Janis Palabinskis, Victor Pashynskyi, Marko Pavlovic, Jacek Pietraszek, Imants Plume, Remigijs Pocs, Dina Popluga, Andriy Popov, Pavlo Potapskyi, Jelena Pundure, Oskars Purmalis, Oingxin Ba, Juan David Ramirez, Anton Rassolkin, Donato Repole, Baiba Rivza, Peteris Rivza, Roman Rogatynskyi, Kestutis Romaneckas, Adolfs Rucins, Miroslaw Rucki, Vita Rudovica, S. K. Gaadhe, Delmy L. Salin, Inna Samuilika, Liliya Savchenko, Dainius Savickas, Rogier Schulte, Jaroslaw Selech, Raimunds Selegovskis, Natalija Sergejeva, Viktor Sheichenko, Antin Shuvar, Monika Skowronska, Valerijs Skribans, Stasys Slavinskas, Raisa Smirnova, Jiri Soucek, Uldis Spulle, Normunds Stanka, Walter Steiner, Indulis Straume, Michal Strnad, Iryna Svider, Andras Szeberenyi, Egidijus Sarauskis, Gintvile Simkoniene, Arturas Smaizys, Ruslans Smigins, Tatjana Tambovceva, Mykola Tolstushko, Franciszek Tomaszewski, Elena Tomovska, Adam Ujma, Puspendra Upadhyay, Arnolds Ubelis, Asta Valackiene, Kristine Valujeva, Daina Vasilevska, Oleksii Vasylkovskyi, Kaspars Vartukapteinis, Girts Veigners, Dainis Viesturs, Anna Vintere, Zane Vitolina, Valentin Vladut, Gheorghe Voicu, Oleksandr Voinalovych, Inta Volodko, Natalja Vronska, Olafs Vronskis, shravan koundinya Vutukuru, Fulin Wang, Jacek Wilkowski, Mirosław Wojtyła, Aleksejs Zacepins, Oksana Zazymko, Raimondas Zemblys, Sandija Zeverte-Rivza, Agris Zimelis, Anda Zvaigzne, Uldis Zaimis.

BEATER-KNIFE CUTTING DEVICES OF FORAGE HARVESTING MACHINES AND WAYS FOR THEIR IMPROVEMENT

Volodymyr Kuzmenko¹, Oleksandr Kholodyuk², Borys Kotov³, Viacheslav Bratishko⁴

¹Institute of Mechanics and Automatics of Agroindustrial Production of the
National Academy of Agrarian Sciences of Ukraine;

²Vinnytsia National Agrarian University, Ukraine;

³Podillia State University, Ukraine;

⁴National University of Life and Environmental Sciences of Ukraine, Ukraine
vfkuzmenko@ukr.net, holodyk76@ukr.net, eetsapk@pdatu.edu.ua, vbratishko@nubip.edu.ua

Abstract. One of the main technological operations in the harvesting of stem fodder is harvesting with simultaneous chopping. Modern round balers, bale balers, and pickup trolleys are equipped with a beater-knife cutting apparatus. They are based on a rotating beater (a pipe with fingers fixed to it) and a number of knives installed in the channel, along which the fingers of the beater move in a rotational motion. In the process of developing the design of such a cutting apparatus, the beater has evolved from an analogue of a scraper-finger conveyor, a rotor with a controlled rake, into a rotor with a tubular shaft and fixed curved fingers radial to its base. The problem with such cutting machines is a significant increase in friction forces on the side surfaces of the knives with an increase in their number. The increase in the number of knives is caused by the need to reduce the length of the raw material to be cut. The research is aimed at determining the design features of the beater-knife cutting units of forage harvesters, the directions of their improvement by replacing the passive knife with an active disc knife and experimentally determining the effect of the circular speed of the knives on fuel consumption. The monographic method was used in the research. This made it possible to systematize the main design parameters of the beater-knife cutting machine, identify the main works carried out in the study of similar designs, and propose a technical solution that can significantly reduce the friction forces that occur on the side surface of the knives. By varying the distance between the knives of the prototype cutting machine, the weighted average cutting length of the resulting raw material was determined. The results obtained made it possible to determine the ratio between the dimensions of the cutting device (which are in the range of: length – 1120-2000 mm, diameter - 415-880 mm, minimum cutting length - 22-25 mm), experimentally confirm the performance of the cutting device with disc knives, establish the dependence of fuel consumption for picking up, cutting and feeding alfalfa on the circular speed of disc knives, and determine the minimum fuel consumption, which is 0.74 kg·h⁻¹.

Keywords: cutting, plant raw materials, beater-knife cutting machine, linear dependence, fuel consumption.

Introduction

Cutting of stem crops is the main operation in the preparation and feeding of stem forage. It is performed when mowing grasses, chopping raw materials during hay, haylage and silage harvesting and when preparing feed before it is distributed. Drum and disc cutters are widely used in forage harvesters. However, with the development of technical means for harvesting grasses and collecting grain straw, beater-knife cutting machines are becoming more common, which are used in balers, bale balers, and pick-up trolleys, the main characteristics of which are shown in Table 1. They organically combine the processes of transporting and cutting stalks. The cutting process and its various aspects have been studied by many authors, but even today, due to the diversity of stalk crops, variation in cutting conditions, development of new and improvement of existing cutting machines, there is a need to study certain aspects of this process. Thus, due to the need for cutting during energy cane harvesting and reducing the size of the cutting apparatus, the effect of the blade inclination, cutting speed, and stem diameter on the specific cutting energy was investigated [1]. The specific cutting energy obtained for different parameters ranged from 0.26 J·mm⁻² to 15.0 J·mm⁻². It is concluded that optimising the cutting speed and blade angle can lead to significant savings in the cutting energy while improving cutting quality.

The authors of [2] studied the effect of the angle of inclination of the blade to the stem during unsupported cutting at three height levels. The angle of inclination of the blade to the stem was varied from 0° to 60° every 15°. It was found that the peak cutting force per unit area of the stem decreased with increasing cutting angle of the blade slide. When cutting without support, the minimum average cutting energy was 9.12 J·mm⁻¹2 at a sliding angle of 45°. When cutting with support, the cutting energy per unit area of the stem ranged from 6.57 to 12.54 J·mm⁻², and the peak cutting force per unit area of the stem varied from 2.46 to 0.98 N·mm⁻². It was concluded that the optimum cutting sliding angle was

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45° when cutting without support and 30° when cutting with support.

In the work [3], the bionic principle of constructing the geometry of the cutting element was used to reduce energy consumption and reduce the effort for cutting corn stalks. The jaw profile of the leaf beetle was experimentally determined with the fourth-degree curve approximation. Based on this profile, a cutting element with a bionic working edge was developed. Comparison of forces and energy consumption for cutting corn stalks with a cutting element with a typical edge profile showed that the average maximum cutting force and energy consumption for cutting for the bionic blade were reduced by 12.89% and 10.73%, respectively. This confirms the prospects of using cutting elements with a bionic cutting edge.

Table 1

Main parameters of beater-knife cutting machines for cutting stem raw materials

| Manu- | | Working | Feed rotor | Number of | Theoretical | Required |
|-----------|-----------------------|-----------|------------------|----------------|-------------|-------------|
| facturer | Model | width, m | diameter/worki | knives, pcs. | cutting | aggregation |
| (brand) | | | ng length, mm | Kilives, pes. | length, mm | power, kW |
| | | | rolleys-pickers | | | |
| Claas | Cargos 8000 | 2.0 | 860/1580 | 40 | 38 | |
| Ciaas | 9000 | 2.0 | 860/1580 | 40 | 38 | - |
| Pottinger | Boss Junior | | | 12 | 120 | 15-44 |
| | Boss | 2.0 | -/- | 31 | 43-172 | 51-96 |
| | Faro | 2.0 | - /- | 31-11 | 45-135 | 66-110 |
| | Jumbo | | | 48-65 | 34-25 | 147-368 |
| Krone | AX | 1.8 | 760/1500 | 16/32 | 90/45 | 59-74 |
| Krone | ZX | 2.12 | 880/1910 | 24/48 | 74/37 | 155-175 |
| Dayamann | Royal | 1.94 | 600/1428 | 41 | 34 | 59-132 |
| Bergmann | Carex | 2.05 | 850/1470 | 41 | 35 | 110-257 |
| Malone | Trojan MT 35 MT 52 | 2.0 | -/2000 | 35 | 40 | 64 97 |
| Roc | CT | - | -/2000 | 18 | - | - |
| | | La | arge-bag pickers | | | |
| Class | QUADRANT 5300 | 2.35 | -/1120 | 51, 26, 13, 12 | 22, 44, 88 | - |
| Claas | 4200 RC | 2.35 | 500/1200 | 25, 13, 12, 6 | 44, 88 | - |
| | BIG Pack 890 XC | 1.95/2.35 | 550/800 | 16, 8 | 44, 88 | 95 |
| Krone | 1270 VC | 2.35 | 550/1200 | 51, 26 | 22 | 135 |
| | 1290 HDP II XC | 2.35 | 720/1200 | 26, 13 | 44, 88 | 190 |
| New | Bigbaler 870 | 1.96 | -/- | 6 | 114 | 80 |
| Holland | 1290 CropCutter | 2.35 | -/1200 | 29, 15 | 39, 78 | 110 |
| 171 | SB 890 | 2.30 | -/1200 | 15 | min 45 | 88 |
| Kuhn | SB 1290 iD | 2.30 | -/1200 | 23, 12, 11 | min 45 | 141 |
| | | | Roll pickers | | | |
| | Fortima 1250 MC | 2.05 | 415/1200 | 17, 15, 7 | 64 | 36 |
| Krone | VariPack V 165XC | 2.15 | 530/1200 | 17, 9, 8 | 64, 128 | 67 |
| | V 190 XC Plus | 2.15 | 530/1200 | 26, 13, 13 | 42, 84 | 74 |
| Claas | ROLLANT 620RC | 2.10 | -/1200 | 25, 15, 14 | 44, 70 | - |
| Claas | 455 RC | 2.10 | -/1200 | 25, 13, 12 | 44, 70 | - |
| Dattingan | Impress F 3130F | 2.05/2.30 | 650/1200 | 16, 8, 8 | 72 | 59 |
| Pottinger | 3160V PRO | 2.30 | 650/1200 | 32, 16, 16 | 36 | 59 |
| New | Roll-Belt 150 | 2.30 | 455/1400 | 15 | 65 | 75 |
| Holland | 190 CropCutter | 2.30 | 520/1400 | 25, 12, 13 | 41, 83 | 88 |
| | Roll Baler | 2.20 | /1220 | 14, 7, 7, 4 | min 70 | 65 |
| Kuhn | FB 3135 | 2.30 | -/1220 | 23, 12, 11, 7 | min 45 | 65 |
| | VBP 2295 | 2.30 | -/1200 | 23, 14 | 45, 70 | 68 |

Machine development requires not only knowledge of individual processes, but also the coordination of individual units. An example of coordinating the operation of a drum cutting machine

and a roller feeder is given in the study [4]. The study solved the problem of ensuring a uniform productive supply of stem feed by a five-roll feeder and high-quality cutting by a drum chopper. The authors determined the profile of the ellipsoidal cutting edge of the knife installed obliquely to the cutting drum. It has been established that the rational parameters of the feeding and cutting apparatus are the feed speed of $3.39~\rm m\cdot s^{-1}$, the rotational speed of the chopping drum of $1016.17~\rm rpm$, the feed rate of $8.04~\rm kg\cdot s^{-1}$, and the deviation of the direction of feeding into the drum from the radial direction of 52.2° . At the same time, the cutting length of the raw material was 95.35% of the specified one, and the energy consumption for the process was $37.63~\rm kJ/kg$.

The development of forage harvesting machines has led to the creation and use of beater-knife cutting machines that organically fit into the technological scheme of picking up and feeding grass mass to the compaction chambers of baling and bale balers and the bodies of pickup trolleys. In the process of developing the design of such a cutting apparatus, the beater has evolved from an analogue of a scraper-finger conveyor (a rotor with a controlled rake) into a rotor with a tubular shaft and fixed curved fingers, radial at its base and deviated against the direction of rotation at the top [5]. At the same time, the blades of the knives were transformed from rectilinear to curved sickle-shaped, with double-sided sharpening (Fig. 1). The knives are installed in one or more rows at the bottom of the beater for transporting stem feed on a special beam. Each knife is spring-loaded and can be deflected to avoid damage if foreign hard objects hit the cutting unit. If the beams in early designs of cutting machines were only tilted downward during maintenance, modern designs allow the beams to be removed from under the cutting machine.

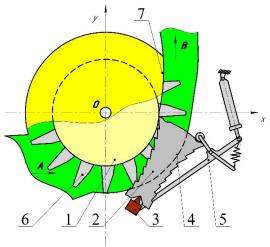


Fig. 1. Scheme of a modern beater-knife cutting machine (cross-section): 1 – beater; 2 – knife; 3 – beam for installing knives; 4 – pallet; 5 – knife springing mechanism; 6 – beater finger; 7 – upper plate of the channel for movement of cut raw materials

The rotors of the cutting machines have a length that corresponds to the design features of the machine on which they are installed. During operation, the rotor fingers pass alongside the knife to ensure high-quality cutting. In some modern models of machines, the fingers are doubled, and they pass simultaneously on both sides of the knife. The length of the fingers reaches of up to 150 mm. It is close to radial in shape at its base and is deflected against the direction of rotation at the tip. This shape ensures that the raw material is pressed against the bottom of the cutting machine and the blade exits the cut mass, which is pushed through the discharge channel.

The cutting machine has a system of individual knife springing, which, if necessary, simultaneously serves to remove them from the stalk mass transportation channel. During operation, the roll of dried or dry grass is fed by the pickup in the direction indicated by the letter A (Fig. 1). The rotor 1, rotating counterclockwise, captures the mass with fingers 6 and directs it to the channel formed by the cylindrical surface of the rotor 1 and the pallet 4. Pulling the mass through the channel, the fingers 6 direct it to the knives 2, which block the channel from the pallet 4 to the rotor surface. The knives are supported by a rigidly mounted beam 3, to which the levers of the knife spring mechanism 5 are connected. The mass flow is cut into separate strips and pushed into the discharge channel (direction B) by the fingers 6. The fingers 6 exit the discharge channel through slots in its upper plate 7.

The difference between the cutting apparatus, the design of which is considered, and the drum and disk cutting apparatus widely used in forage harvesting is that cutting occurs in the longitudinal plane of the raw material flow, which is divided into separate, narrowed flows by cutting elements. In this way, the cutting length can be adjusted by changing the distance between the installed knives, while in a drum or disk cutting machine, the cutting length is regulated by the speed of the feed rollers.

Smooth operation of the cutting apparatus is ensured by the alternate operation of each of the knives and sliding cutting, which is the result of using knives with a curved blade. By modelling the shape of the knife blade and checking it experimentally, it was found [6] that the use of the developed knife blade profile reduces the specific cutting force, which leads to a decrease in the fuel consumption. It has also been confirmed that the smoothness of the cutting apparatus has increased, and the resulting stem feed meets the requirements of modern livestock production.

The determination of energy consumption by a beater-knife cutter (rotary feeding and cutting system – RFCS) during straw cutting in a combine harvester is the subject of works [7; 8]. To do this, the physical and mechanical properties of the raw material were determined under the conditions of the cutting apparatus, and experimental studies were conducted. A model has been developed that allows determining energy consumption when changing the parameters and operating modes of the cutting unit.

When developing a multifunctional forage harvester [9], the distribution of forces and deformations of the rotor of a beater-knife cutter were analysed by means of finite element modelling (Autodesk 2015). It was found that for the proposed design, the safety factor is 3.97, which significantly exceeds the standard value of 2.6 for maximum load. The maximum strain and stress values were 1.8 mm and 172.39 MPa, respectively.

Along with the positive characteristics of the above-mentioned beater-knife cutting machine, it also has disadvantages. To achieve minimum cutting lengths, the knives are installed at a small distance from each other. In this regard, the cost of friction on the side walls of the knives increases significantly, and the energy demand during the operation of the cutting machine increases.

Materials and methods

The monographic method was used during the research. This made it possible to identify the main works carried out in the study of similar structures, to systematize the main design parameters of the beater-knife cutting machine and to propose a technical solution that can significantly reduce the friction forces that occur on the side surface of the knives. The design and construction approach was used to develop a prototype of the cutting apparatus, which was installed on a roll picker and used in field experimental studies.

The picker equipped with a disk cutting unit was tested on alfalfa swaths of the second cut with a moisture content of 44.7-52.3%. The weight of a running meter of swath ranged 2.37-3.84 kg·m⁻¹. The picker was combined with a tractor and a 45 m3 trailer. The tractor speed ranged 5.35-5.42 km·h⁻¹ (1.49 to 1.51 m·s⁻¹). The direction of rotation of the disk knives helped move the mass of alfalfa. The disk knives with a diameter of 500 mm, a thickness of 3.0 mm and a weight of 5.3 kg had chamfers sharpened at an angle of 29-30°. The design features of the rake and the stiffening ribs of the channel plane allowed the discs to be installed at four different distances: 100, 190, 200, and 270 mm from each other. Samples of the cut mass were taken from each respective strip, and disassembled by length, and the weighted average cutting length was determined based on the information obtained. The circular speed of the cutting edge of the circular knives was 5.34, 7.70, and 12.82 m·s⁻¹. The change in the circular speed was achieved by changing the driven sprockets on the shaft of the disk knife battery. The circular speed of the disk knives was higher than the average speed of pushing the mass through the channel (0.68 m·s⁻¹). The average cutting length of the stem raw material particles was determined according to [10; 11].

Results and discussion

A significant step forward in the technical development of the design of the beater-knife cutting machine was made when the IMPRESS round baler was created [12]. Due to the transportation of the raw material flow by the rotor during its clockwise rotation, the knives are located above the rotor instead of below. This ensures that the direction of feeding the raw material flow into the bale chamber coincides

with the direction of movement of the bale surface, which reduces energy consumption for bale formation. The increased space for the knives allows for the installation of 32 knives at a distance of 1.2 m, which provides a design cutting length of 36 mm. The extension to the left side of the beam to install the knives at a height of about 1.2-1.4 m makes it much easier to replace or rotate the knives on it.

Having processed the information of manufacturers and scientific and technical literature [13-19], the main parameters of the beater-knife cutting machines used in stem forage harvesting machines were systematized. Some of the results obtained are summarised in Table 1. Its analysis shows that the working width of forage harvesters ranges from 1.8-2.3 m, with smaller values being typical for earlier machines. The length of the rotor corresponds to the size of the chamber into which the cut mass is fed. The smallest values are in round balers (bale height 1.0-1.2 m), the largest – in trolley balers – up to 2.0 m. Accordingly, the rotor diameters are larger in longer rotors and reach 880 mm. The pitch of the fingers on the beaters is smaller in modern designs, which ensures a more even supply of raw materials to the knife. A graphical interpretation of the relationship between the beater length and diameter is shown in Fig. 2.

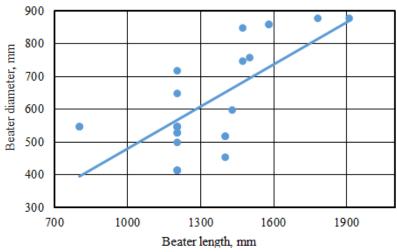


Fig. 2. Dependence of the cutting machine beater diameter on its length

Figure 2 shows that most cutters have a length of 1200 mm (the height of bales formed by bale balers) and 1400-1500 mm (one side of the cross-section of large bales). Increasing the length of the beater leads to an increase in its diameter, and, accordingly, to an increase in the ability to push the raw material through. However, the directions of development of the cutting machine do not solve the problem of reducing the friction of raw materials on the side surfaces of the knife. We proposed a cutting machine with rotating disk knives [20]. This reduces friction forces. The disks are arranged in two or three rows and are assembled on shafts. Each battery is mounted on rolling bearings, spring-loaded and has an individual drive. A special feature of the picker used to test the technological process of cutting with circular knives is the transportation of the selected raw materials by pushing. The raw material is pushed by a packer, the edges of the tine fingers of which move along an ellipsoidal closed path. The knives were installed outside across the plane inclined to the horizon at an angle of 60° (Fig. 3), which feeds the raw material to the discharge channel.

During the study of fuel consumption during the process of picking up raw material rolls, cutting them and transporting them, the disc knives rotated in the direction of raw material movement. The fuel consumption was measured when the machine was running at idle. The dependence of fuel consumption for the feeding and cutting process on the circular speed of the circular knife is shown in Fig. 4. The resulting dependence is well described by a linear function, with the reliable approximation value $R^2 = 0.982$.

Fig. 4 shows that reducing the knife edge speed to the value of the mass transportation speed leads to a decrease in fuel consumption for the process. This is due to an increase in the cost of friction of the mass on the surface of the disk with an increase in the relative speed of the mass on the disk. The minimum fuel consumption is achieved when the knife battery operates without a drive. In this case, the rotation of the disks is achieved due to the cutting forces acting on the edge of the knife and the friction forces acting on the side surface of the knife. It was also found that the costs directly related to the

process make up only 9.0-12.8% of the total fuel consumption by the unit.

The research results [21], which relate to the ratio of the distance between the knife disks and the actual average cutting length, show that the latter is 1.2-1.4 times greater than the distance between the knives. This is due to the arrangement of alfalfa stalks in the flow at the time of feeding to the disk knife.

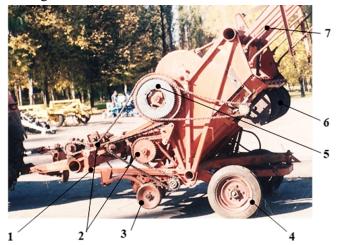


Fig. 3. General view of the swath picker (without protective shields and the lower tray of the discharge channel): 1 – frame, 2 – picker and packer drive, 3 – surface tracking picker wheel, 4 – support wheel, 5 – knife battery drive, 6 – disk knife battery, 7 – discharge channel

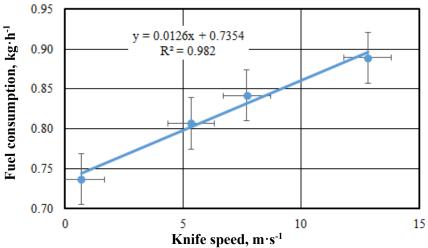


Fig. 4. Dependence of fuel consumption for the process of picking up, feeding and cutting mass depending on the circular speed of the cutting edge of a circular knife

This arrangement is formed by the tines of the rake, which push the raw material through. However, the arrangement of the stalks in the swath should also be taken into account. The latter depends on the operations performed on the swath: whether it is only mowing with simultaneous swath formation or moving the swath at the same time as raking. The pick-up operating parameters also affect the way the stalks are arranged.

Conclusions

- 1. The dimensions of the beater of the cutting machine correspond to the design features of the machine on which it is installed and vary within the following limits: length 1120-2000 mm, diameter 415-880 mm. The pitch of the beater pins along its length corresponds to the maximum possible number of knives to be installed to ensure backup cutting. In modern designs, the pitch of the pins around the circumference of the drum of the beater reaches the minimum value for uniform feeding to the knife in small portions. The minimum cutting length is determined by the distance between the knives and has reached 22-25 mm.
- 2. The circular blade reliably performs the cutting process while minimizing energy losses due to

- friction on the blade side surfaces. Thanks to the circular shape of the cutting edge, its sharpness can be maintained with a sharpening mechanism with minimal time spent.
- 3. Minimum fuel consumption of 0.74 kg·h⁻¹ for picking up, cutting, and feeding alfalfa using disk knives is achieved at a circular speed close to the speed of alfalfa transportation in the canal.

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