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Contents

| ~ 1 | NO ALL Makidus P. OARKER, Absord ARRIU IRRAUM, Respirit NOUAMER, A Link Onis Veriable Reset RO DO Occurrence for | |
|----------|--|------------|
| 01 | M.S. ALI, Manidur R SARKER, Anmad ASRUL IBRAHIM, Ramizi MOHAMED - A High Gain Variable Boost DC-DC Converter for | 1 |
| 02 | Abdelkader Abdallah, Abdelkader Chaker, Tayeb Allaoui - An adaptive RST fuzzy logic and an adaptive PI fuzzy logic controllers of | 11 |
| 03 | Tadeusz PIETKIEWICZ, Patryk DUDEK - Comparison of maritime objects recognition efficiency upon FLIR images using neural | 21 |
| 04 | Ahmed Jamel Abdullah Al-Gburi, Imran Bin Mohd Ibrahim, Zahriladha Zakaria,. Nur Farzana Bt Mohd Nazli - Wideband | 26 |
| 05 | Mowafak K. Mohsen, Ayad Hameed Mousa, Rawya Read Jowad - New design of low profile Uniform Substrate integrated | 30 |
| 06 | Pichaya CHAIPANYA, Nuchanart SANTALUNAI, Samran SANTALUNAI - A design of a single element switched beam antenna on Muchanam like EPC structures | 35 |
| 07 | Syah ALAM, Indra SURJATI, Lydia SARI, Atria ANINDITO, Agam Yudi PUTRANTO, Teguh Firmansya - Bandwidth Enhancement | 40 |
| 08 | MANSUR, Salama MANJANG, Ardiaty ARIEF, Yusri Syam AKIL - Hybrid renewable energy generation planning for isolated microard in Indonesia with metabeuristic approach | 45 |
| 09 | Agus SISWANTO, Ansar SUYUTI, Indar CHAERAH GUNADI, Sri MAWAR SAID - Steady-State Stability Limit (SSSL) Assessment when Wind Turbine Penetration to South Sulawesi System Using ANN | 51 |
| 10 | Sanchai EARDPRAB, Tajchai PUMPOUNG - Designing LabVIEW Application for Impedance Measurement by using Differential Probe | 57 |
| 11 | Thanat NONTHAPUTHA, Montree KUMNGERN - CMOS Single Input Multiple Output Universal Biquad Filter Current-Mode Using Only OTAs | 64 |
| 12 | Ameur Fethi AIMER, Ahmed Hamida BOUDINAR, Mohamed Amine KHODJA, Azeddine BENDIABDELLAH - Frequency resolution improvements in induction motor fault diagnosis : Experimental validation | 69 |
| 13 | Nazar Jabbar Alhyani, Oday Kamil Hamid, Sarah yahia Ali, Ayman Mohammed Ibrahim - Efficient Terrestrial Digital Video Broadcasting Receivers Based OFDM Techniques | 74 |
| 14 | Narongchai Thodsaporn, Vijit Kinnares, Papol Sardyoung Grid Connected Unsymmetrical Two-Phase Induction Generator System Using Time-Based Unbalanced Space Vector PWM and Adaptive Hysteresis Band Current Control | 78 |
| 15 | Elena Sosnina, Andrey Shalukho, Leonid Veselov - The SOFC in the Hybrid Power Supply System of a Livestock Enterprise | 89 |
| 16 | NEKROUF Sadek, CHEKROUN Soufyane - Optimal controller design for a birotor helicopter | 93 |
| 17 | TABTI Khatir, MOSTEFAI Lotfi, CHEKROUN Soufyane, LARBAOUI Ahmed - Electric vehicle yaw moment control based on the body sideslip estimation | 97 |
| 18 | Weera RATTANANGAM, Chuthong SUMMATTA - Relay Drive Circuits for a Safe Operation Order with a Digital Logic ICs Sequential Switching Function | 102 |
| 19 | Murat ASANOV, Salima ASANOVA, Murodbek SAFARALIEV, Egor LYUKHANOV, Alexander TAVLINTSEV, Stanislav SHELYUG - Elementwise power losses calculation in complex distribution power networks represented by hierarchical-multilevel topology structure | 106 |
| 20 | Szczepan PASZKIEL, Ryszard ROJEK, Ningrong LEI, Maria Antonio CASTRO - Review of solutions for the application of example | 111 |
| 21 | Ernest BRZOZOWSKI, Oskar SADOWSKI, Paweł GÓRECKI, Krzysztof GÓRECKI, Ryszard KISIEL, Marek GUZIEWICZ - Fvaluation of Assembly Technology of IGBT Mounted not TO-220 by Durability Tests | 117 |
| 22 | Jacek Maciej STANKIEWICZ - Selection of load impedance in order to maximize the receiver power in the periodic WPT system | 122 |
| 23 | Robert Grolik, Michał Góra, Mateusz Góra, Mateusz Dyląg - A study of the influence of external factors on the temperature control | 128 |
| 24 | process of a 3D printer nead in FDM technology | 122 |
| 24 25 | Artur SZCZĘSNT, Adam GRACZTR - Lew current transducer as an alternative for Pertaint current transdomer in RCD protection Tomáš ŠKIIMÁT Žanata El ESCHOVÁ - Negative Sequence Current as a Prakter Failure Protection for Medium Voltane Grid | 136 |
| 26 | Oleksandr SHAVOLKIN, Irvna SHVEDCHYKOVA, Svitana DEMISHONKOVA, Volodymyr PAVLENKO - Increasing the efficiency | 144 |
| | of hybrid photoelectric system equipped with a storage battery to meet the needs of local object with generation of electricity into grid | |
| 27 | Michał PIEKARZ - The analysis of the wind generation impact on the power system stability | 150 |
| 28 | Tomasz KOTLICKI - Energy efficiency of power plant auxiliaries | 154 |
| 29 | Sebastian LACHECINSKI - Support of temporal data for the transaction time on the ORACLE platform | 159 |
| 30 | Hatem Mohammed Naguib Fiyad, Ahmed Gamal Abdellatif, Adel Zaghloul Mahamoud, Mostafa Mohamed Ahmed, Mohamed E | 164 |
| 31 | Ajay Vasanth. X, P. Sam Paul, D. S. Shylu, P. Mano Paul - IoT based prognostics using MEMS sensor with single board computers | 170 |
| 32 | for rotary machines Shatha Y. Ismail ¹ , Zozan Saadallah Hussain, Hassaan TH. H. Thabet, Mohamad Mo.Z.M. Amin, Thabit H. Thabit - Design and | 175 |
| 33 | Simulation of an Adaptable Pulsating Irrigation System Using Programmable Logic Controller Unit Ihor Kupchuk, Vitalii Yaropud, Valerii Hraniak, Julia Poberezhets, Oleksii Tokarchuk, Volodymyr Hontar, Andrii Didyk - | 179 |
| 34 | Multicriteria compromise optimization of reed grain grinding process M.S. ALI, Mahidur R SARKER, Ahmad ASRUL IBRAHIM, Ramizi MOHAMED - High Efficiency Flywheel Motor Generator Model with | 184 |
| 35 | Hussam Keriee, Mohamad Kamal A. Rahim, Osman Ayop, Nawres Abbas Nayyef, Ahmed Jamal Abdullah Al-Gburi, B.A.F Ermail Synd Muzabir, Abbas - Widebard Planar Microstrin Antenna Based on Split Ping Personator For 5G Mobile Applications | 190 |
| 36 | Anis Jouini, Azer Hasnaoui, Fethi Mejri, Adnane Cherif, Salem Hasnaoui - A Real time Software Tool for 2D/3D Antenna Radiation Pattern | 195 |
| 37 38 | Salem GAHGOUH, Imen SAIDI, Ali GHARSALLAH - Optimal study and analysis of the directivity of acoustic antennas multi-sensors Tomasz NACZYŃSKI, Roman KORAB - Possibilities of forming the electricity balance of an individual customer equipped with a | 199 203 |
| 39 | photovoltaic source Yuriy SAYENKO, Ryszard PAWEŁEK, Vadym LIUBARTSEV - Wind power forecasting based on meteorological data using neural | 207 |
| 40 | networks | 044 |
| 40 | Dariusz Swigulari - Higner Schools teaching Polish electrical engineers before World War II | 211 |

1. Ihor Kupchuk, 2. Vitalii Yaropud, 3. Valerii Hraniak, 4. Julia Poberezhets, 5.Oleksii Tokarchuk, 6. Volodymyr Hontar, 7. Andrii Didyk

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Multicriteria compromise optimization of feed grain grinding process

Abstract. Optimization of the feed grinding process by a vibrating rotary crusher was carried out and shown in the article: a multifactor experiment was carried out, a statistical analysis of the results was carried out using the software "Statistica 10.0", mathematical models were obtained in the form of multiple regression of the second order and their adequacy was checked by the Fisher criterion. Rational operating parameters were obtained by Cramer's method using the "Mathcad 15.0" software.

Streszczenie. Przeprowadzono i przedstawiono w artykule optymalizację procesu rozdrabniania ziarna przez wibracyjną kruszarkę obrotową: przeprowadzono eksperyment wieloczynnikowy, przeprowadzono analizę statystyczną wyników za pomocą programu "Statistica 10.0", modele matematyczne uzyskano w forma regresji wielokrotnej drugiego rzędu i ich adekwatność sprawdzono za pomocą kryterium Fishera. Racjonalne parametry pracy uzyskano metodą Cramera przy użyciu programu "Mathcad 15.0". (Wielokryterialna optymalizacja procesu mielenia ziarna paszowego)

Keywords: statistical analysis, multifactor experiment, rotatable central-compositional planning, functional dependence. **Słowa kluczowe:** optymalizacja, kruszenie ziarna, , optymalizacja wielokryterialna.

Introduction

Feeds make up most of the cost of livestock products and determine its quality, and one of the most important and energy-intensive operations is grinding of grain, especially substandard (wheat, barley, peas, corn, etc.) [1, 2]. The need for grinding grain feed is conditioned by the physiological characteristics of animals [3, 4], as the rate of processing feed with gastric juice is directly proportional to its surface area [5, 6]. At the same time, in the technological process of feed preparation, the share of energy consumption for grinding can reach 65% [2, 7, 8]. Therefore, the effective functioning of farms in modern conditions requires development and implementation of technologies that meet international standards and reducing energy intensity of the process is an urgent task.

Analysis of literary sources and problem statement

To reduce the energy intensity of this process the experimental model Vibrating-Rotor Crusher [7, 9, 10] has been developed, in which the combination of grinding methods (impact and cutting) makes it possible to process substandard raw materials with a high moisture content while reducing energy consumption for this technological operation [8].

On the base of the Department of Technological Processes and Equipment for Food and Processing Industries of Vinnytsia National Agrarian University laboratories the ranges of amplitude-frequency characteristics of Vibrating-Rotor Crusher on the angular velocity of the drive shaft were researched [11].

However, in order to achieve high energy efficiency, it is necessary to substantiate the rational modes of operation for the suggested equipment for established ranges.

Purpose and tasks of research

The purpose of the article is to substantiate energyefficient and resource-saving modes of operation of the vibratory disk crusher based on the analysis of quality and energy performance of the process of grinding feed grain. To achieve this goal, it is necessary to performed the multifactors experiments to change the dispersed properties of the processed material (corn) under the action of impactcutting action of the disk-type beaters.

Materials and methods

Experimental part of the work was performed on the base of the Department of Technological Processes and Equipment for Food and Processing Industries of Vinnytsia National Agrarian University laboratories on the stand (Fig. 1) and experimental model of the vibratory crusher [9, 11]. The first part of the experimental research was based on the analysis of the amplitude-frequency characteristics [11, 12] of the actuator and the consumed energy [8, 13, 14] for driving the machine. The second part was devoted to the determining the technological parameters of the studied process, in particular the assessment of the equipment performance [7] and dispersion of the obtained material [15].

Comprehensive statistical analysis [16, 17] of those parameters allows finding rational modes of the machine operation, which provide maximum efficiency of the process of grinding grain while ensuring the desired dispersion of the finished product.



Fig. 1. Experimental stand: 1 – experimental sample of the vibratory disk crusher; 2 – personal computer; 3 – switch; 4 – EMF-1 electronic wattmeter; 5 – secondary electromechanical wattmeter; 6 – AOCH-20-220-75 laboratory transformer; 7 – accelerometer.

To record the amplitude-frequency characteristics of the vibratory disk crusher, a sensor based on the ST Microelectronics LIS3DH accelerometer was developed (Fig. 2) [11, 18].

In order to register the frequency of the drive shaft a wireless tachometer UNI-T UT372 (Fig. 3a) was used, the principles and procedures of operation of which are described in the technological documents [7, 11].



Fig. 2. Accelerometer (general view of the device): 1 – microport for the accelerometer sensor connection; 2 – power supply battery; 3 – memory card; 4 – power button; 5 – adaptive microport for data reading; 6 – accelerometer housing

To control and change the rotation speed of the electric motor shaft autotransformer AOCH-20-220-75 (Fig. 3b) was used designed to work with alternating current [7, 8, 11].



Fig. 3. Devices for velocity control of the drive shaft:

a) UNI-T UT372 frequency meter: 1 – laser reader; 2 – digital indicator; 3 – control panel;

b) AOCH-20-220-75 laboratory autotransformer: 1 – outer casing;
2 – voltage regulators; 3 – input and output terminals.



Fig. 4. Devices for research the technological parameters: a) EMF-1 electronic wattmeter: 1 – wattmeter housing; 2 – control panel; 3 – indicator display.

a) PG-2 vibrating feeder: 1 – loading hopper; 2 – sliding shutter; 3 – electromagnetic vibration excitor; 4 – conveying tray; 5 – springs; 6 – unloading neck.

c) Wile-55 moisture meter: 1 – case cover; 2 – digital indicator; 3 – control panel; 4 – test sample container.

d) A-20 sieve analyzer: 1 - vibrating platform; 2 - sieve block;

3 – fixing screws; 4 – dustproof surface; 5 – control panel.

To determine power characteristics the EMF-1 electronic wattmeter was used (Fig. 4a) [8]. The device measured the following parameters: utility supply voltage, frequency and power of alternating current, the consumed power, coefficient of performance (100% for active load), equipment operating time and total power consumption for the whole period of the machine operation (kW/h).

The crusher separation surface perforation diameter was changed by installing appropriate sieves with round holes of the following sizes: d=1 mm; 1.25 mm; 1.4 mm; 1.6 mm; 1.8 mm; 2 mm [9].

To change the mode of the feed-in of the material PG-2 mobile vibrating dispenser was used (Fig. 4b) [19], in which the loaded into the hopper 1 material through the unloading hole, partially closed by the sliding shutter 2, falls on the tray 4 and under the forced oscillation action of the latter, caused by electromagnetic vibrator 3, moves along it and is unloaded through the neck 6.

To determine the moisture content of the material a Wile-55 moisture meter (Fig. 4c) was used, intended to measure the relative humidity of various types of grains and seeds, characteristics of which are stored in the device memory [8].

Productivity evaluation was done by weighing the crushed material that passed through the crusher over a time interval [7].

Dispersity of the material was determined by the method of mechanical separation of particles – sieve analysis. The experimental material was passed through the A-20 laboratory sieve analyzer (Fig. 4d) [15]. Sieves with a hole size of 1; 0.8; 0.6; 0.4; 0.2 mm were used.

For the quality assessment of the crushed material, the rate of extraction or the proportion of its passage through the control sieve was assumed [20]. By extraction we mean the number of particles in the product after grinding, expressed as a percentage over weight of the sample taken for the analysis. The technology of feeding farm animals suppose the dispersion of the compound feed particles in the range of 0.5-3.5 mm, depending on the animal kind, age and method of keeping [1]. Given the ability of a vibratory disc crusher to obtain particles of different sizes, as a control indicator of the quality of grinding we took the following conditions: the finished product particle size should not exceed 1 mm [2, 3]; the proportion of the material with particle size not more than 1 mm should be not less than 85% of the total weight of the crushed product [4].

Statistical analysis of the experimental data array, aimed at receiving functional dependence in the form of multiple regression of the second order was obtained using rotatable central-compositional planning (RCCP) of a multifactorial experiment [21]. The RCCP method makes it possible to obtain a more accurate mathematical description of the data distribution by increasing the number of experiments at the central points of the plan matrix and a special choice of the "star value" [18]. Processing of the experimental data was carried out in the statistical environment "Statistica 10.0." and "Mathcad 15.0" [21].

Qualitative and energy parameters of optimization of the studied process are determined as: productivity P, kg·h⁻¹; specific passage through the control sieve (holes diameter d_c=1.0 mm) K, %; consumed energy N, W. Based on our own experience [2, 7, 8, 11, 12] and having analyzed other scientists research results [1, 5, 6, 10, 19], vibration acceleration a, m·s⁻²; the separation surface holes diameter d, mm; amount of the material feed-in Q, kg·h⁻¹; moisture content of the material M,% are determined as the factors that have the greatest impact on the defined optimization parameters:

| (1) | P=f(a, Q, M, d); |
|-----|------------------|
| (2) | K=f(a, Q, M, d); |
| (3) | N=f(a, Q, M, d). |

The number of factors (RCCP) is:

(4)
$$k=k_c+2n+k_0$$
,

where k_c is the number of factors in the core of the plan; n – number of factors; 2n – the number of studies in "star points"; k_0 – the number of factors in the center of the plan with coordinates (0.0... 0). The rotatability of the compositional plan is acquired provided that the size of the

star arm α is selected from the interval $\alpha = 2^{\frac{1}{4}}$ at $n \le 5$, i.e. for a four-factor experiment $\alpha = 2$.

All factors included in functions (1-3) are the parameters that have different dimensions and orders. Therefore, in order to obtain the response surface of these functions, a factor coding operation was performed, which is a linear transformation of the factor space. The following values of factor levels are set in a conditional scale: minimum "-1", average "0", maximum "+1" and star values "- α ", "+ α ". The true values of the factors of the RCCP matrix are established on the basis of the results of experimental studies described above and are shown in table 1.

Levels of factors Factors 0 -1 +1 + -α α $x_1 - vibration acceleration, m \cdot s^{-2}$ 35 30 40 45 50 x₂ – feed-in, kg·h⁻¹ 200 300 400 500 600 x₃ - material moisture 20 14 17 23 26 content,% 1.4 1.6 2 x_4 – sieve hole diameter, mm 1.2 1.8

Table 1 - Levels of factors and intervals of variation

To carry out the RCPC of a four-factor experiment, a matrix of experiments planning was compiled, which is presented in table 2. It is planned to obtain the 2nd order multiple regression equation [20]:

(5)
$$y = b_0 + \sum_{i=1}^n b_i x_i + \sum_{i=1}^n b_{ij} x_i^2 + \sum_{i=1}^n b_{ij} x_{ij} x_{ij} ,$$

where *y* is one of the qualitative functions, *P*, *K*, *N*; b_0 , b_i , b_{ij} – regression coefficients obtained by the method of least squares.

Table 2 – Four-factor matrix to performed the multifactors experiment (encoded)

| Nº | X 1 | X ₂ | X 3 | X4 | F(x _{1,} x _{2,} x _{3,} x ₄) |
|----|------------|-----------------------|------------|----|--|
| 1 | + | + | + | + | + |
| 2 | - | + | + | + | - |
| 3 | + | - | + | + | - |
| 4 | - | - | + | + | + |
| 5 | + | + | - | + | - |
| 6 | - | + | - | + | + |
| 7 | + | - | - | + | + |
| 8 | - | - | - | + | - |
| 9 | + | + | + | - | - |
| 10 | - | + | + | - | + |
| 11 | + | - | + | - | + |
| 12 | - | - | + | - | - |
| 13 | + | + | - | - | + |
| 14 | - | + | - | - | - |
| 15 | + | - | - | - | - |
| 16 | - | - | - | - | + |
| 17 | +α | 0 | 0 | 0 | 0 |
| 18 | -α | 0 | 0 | 0 | 0 |
| 19 | 0 | +α | 0 | 0 | 0 |
| 20 | 0 | -α | 0 | 0 | 0 |
| 21 | 0 | 0 | +α | 0 | 0 |

| 22 | 0 | 0 | -α | 0 | 0 |
|----|---|---|----|----|---|
| 23 | 0 | 0 | 0 | +α | 0 |
| 24 | 0 | 0 | 0 | -α | 0 |
| 25 | 0 | 0 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 | 0 | 0 |

Research results

The results of experimental studies are shown in table 3. Analysis of the statistical characteristics (table 4) of the obtained data showed that the coefficients of their asymmetry go to zero, i.e. the distribution of experimental data is symmetric and is approximated by the normal law.

The adequacy of the obtained mathematical models was evaluated according to Fisher's criterion, which showed that the calculated values are much lower than the critical ones, thus, the obtained regression models adequately describe the response surfaces and can be used for the investigated process optimization [16, 18].

Table 3 - The results of a multifactorial experiment

| | Variable factors | | Parameters | | | | |
|----|------------------|--------|------------|-----|--------|------|------|
| Nº | a, | Q, | Μ, | d, | Ρ, | К, | Ν, |
| | m·s⁻² | kg∙h⁻¹ | % | mm | kg∙h⁻¹ | % | W |
| 1 | 45 | 500 | 20 | 1.8 | 387 | 80.9 | 1335 |
| 2 | 35 | 500 | 20 | 1.8 | 321 | 70.7 | 928 |
| 3 | 45 | 300 | 20 | 1.8 | 297 | 81.3 | 997 |
| 4 | 35 | 300 | 20 | 1.8 | 271 | 67 | 804 |
| 5 | 45 | 500 | 16 | 1.8 | 455 | 81.2 | 1276 |
| 6 | 35 | 500 | 16 | 1.8 | 311 | 71.2 | 917 |
| 7 | 45 | 300 | 16 | 1.8 | 299 | 81.8 | 935 |
| 8 | 35 | 300 | 16 | 1.8 | 283 | 67.5 | 793 |
| 9 | 45 | 500 | 20 | 1.4 | 343 | 93 | 1570 |
| 10 | 35 | 500 | 20 | 1.4 | 230 | 85.1 | 945 |
| 11 | 45 | 300 | 20 | 1.4 | 279 | 94 | 1186 |
| 12 | 35 | 300 | 20 | 1.4 | 236 | 85 | 854 |
| 13 | 45 | 500 | 16 | 1.4 | 376 | 91 | 1520 |
| 14 | 35 | 500 | 16 | 1.4 | 269 | 86 | 934 |
| 15 | 45 | 300 | 16 | 1.4 | 299 | 91.3 | 1102 |
| 16 | 35 | 300 | 16 | 1.4 | 281 | 86.3 | 867 |
| 17 | 50 | 400 | 18 | 1.6 | 399 | 93 | 1101 |
| 18 | 30 | 400 | 18 | 1.6 | 260 | 72 | 815 |
| 19 | 40 | 600 | 18 | 1.6 | 392 | 93.2 | 1595 |
| 20 | 40 | 200 | 18 | 1.6 | 330 | 93.6 | 877 |
| 21 | 40 | 400 | 22 | 1.6 | 300 | 91 | 1320 |
| 22 | 40 | 400 | 14 | 1.6 | 400 | 95.6 | 1070 |
| 23 | 40 | 400 | 18 | 2 | 398 | 66.7 | 910 |
| 24 | 40 | 400 | 18 | 1.2 | 282 | 94.2 | 1595 |
| 25 | 40 | 400 | 18 | 1.6 | 344 | 93.5 | 1200 |
| 26 | 40 | 400 | 18 | 1.6 | 340 | 93.6 | 1205 |

Table 4 – Statistical characteristics

| Indicator | Parameter values | | |
|-------------------------------|------------------|--------|--------|
| | Ρ, | К, | Ν, |
| | kg∙h⁻¹ | % | W |
| number of factors | 26 | 26 | 26 |
| minimum value | 230 | 66.7 | 793 |
| maximum value | 455 | 95.6 | 1595 |
| average value | 322.4 | 84.6 | 1102 |
| upper limit of the confidence | 345.6 | 88.6 | 1206 |
| interval | | | |
| lower limit of the confidence | 299.1 | 80.7 | 997 |
| interval | | | |
| geometric mean | 317.6 | 84 | 1075 |
| harmonic mean | 312.9 | 83.4 | 1050 |
| median | 305.5 | 86.2 | 1034 |
| mode | 299 | 85.3 | 1595 |
| mode frequency | 2 | 2 | 2 |
| lower quartile | 281 | 80.9 | 910 |
| upper quartile | 376 | 93.2 | 1276 |
| range | 225 | 28.9 | 802 |
| interquartile range | 95 | 12.3 | 366 |
| asymmetry | 0.493 | -0.724 | 0.739 |
| kurtosis coefficient | -0.462 | -0.883 | -0.629 |

After processing the experimental data in the statistical environment "Statistica 10.0.", the coefficients of complex multiple regression equations of the 2nd order were obtained (6-8):

 $\begin{array}{c|c} & & P = 380 - 11.5a - 0.4Q + 7M - 24.8d + 0.24a^2 - 0.5M^2 - \\ (6) & & -11.3d^2 + 0.02aQ - 0.06aM - 5.3ad - \\ & & -0.05QM + 0.16Qd + 16.7Md; \\ \hline & \mbox{for the specific passage:} \\ (7) & & \mbox{K=81.83-1.3a+0.07Q+1.48M+12.62d+0.03a}^2 - 0.05M^2 - \\ & & -3.2d^2 + 0.04aQ - 0.25ad - 1.7Md; \\ \hline & \mbox{for the consumed energy:} \\ & & \mbox{N=1042.7-19.7a-1.5Q-11.2M-78d+0.42a}^2 - 1.05M^2 - \\ (8) & & \mbox{-178d}^2 + 0.096aQ + 0.74aM - 18.2ad - 0.2QM - \\ \end{array}$

-0.8Qd+13.62Md.

The response surfaces for this parametrs are shown in fig. 5, fig. 6, fig. 7.



Fig. 5. Productivity in pair interaction of the main factors: a) vibration acceleration and material feed-in; b) material moisture content and feed-in; c) material feed-in and the separation surface holes diameter; d) vibration acceleration and the separation surface holes diameter.





Fig. 6. Passage through the control sieve in pair interaction of the main factors: a) moisture content of the material and the separation surface holes diameter; b) material feed-in and the separation surface holes diameter; c) vibration acceleration and the separation surface holes diameter; d) moisture content and material feed-in; e) material moisture content and vibration acceleration; f) vibration acceleration and material feed-in.



Fig. 7. Consumed energy in pair interaction of the main factors: a) moisture content of the material and the separation surface holes diameter; b) material feed-in and the separation surface holes diameter; c) material moisture content and feed-in; d) vibration acceleration and the separation surface holes diameter; e) material moisture content and vibration acceleration; f) – material feed-in and vibration acceleration.

The rational values of parameters for grinding process with a vibratory disk crusher were determined by Cramer's method using the "Mathcad 15.0" [21] software (table 5).

Table 5 - Rational values of parameters

| Parameters | Values |
|---|---------|
| Vibration acceleration, m·s ⁻² | 32-38 |
| Material feed-in, kg·h⁻¹ | 342-480 |
| Material moisture content, % | 16-18 |
| Separation surface holes diameter, mm | 1,6-1,8 |

It was also determined that at these parameters the grinding feed grain prosess by the vibratory disk crusher reached compromise values between the criteria of productivity, energy consumption and grinding quality.

Conclusions

According to the results of a multifactor experiment, mathematical models in the form of second-order multiple regression, which adequately describe the studied process, were obtained. The analysis of the obtained models allowed to receive rational mode parameters of the studied process: operating mode of vibration acceleration – a=32... 38 m·s⁻²; geometric parameters of the separation surface – d=1.6...1.8 mm; material feed-in – Q=342... 480 kg·h⁻¹; moisture content of the material – W=16...18 %. In compliance with the specified limits of design and mode parameters, quality and energy characteristics of the process acquire the following values: productivity is 320...450 kg·h⁻¹, specific passage through the control sieve – 85... 95 % at the energy consumption 1.2... 1.5 kW for the crusher drive.

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